

# **SS EL FARO Stability and Structures Preliminary Report Summary**



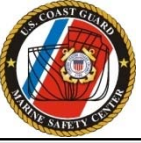
**Jeffrey W. Stettler, Ph.D., P.E.**

**February 6, 2017**

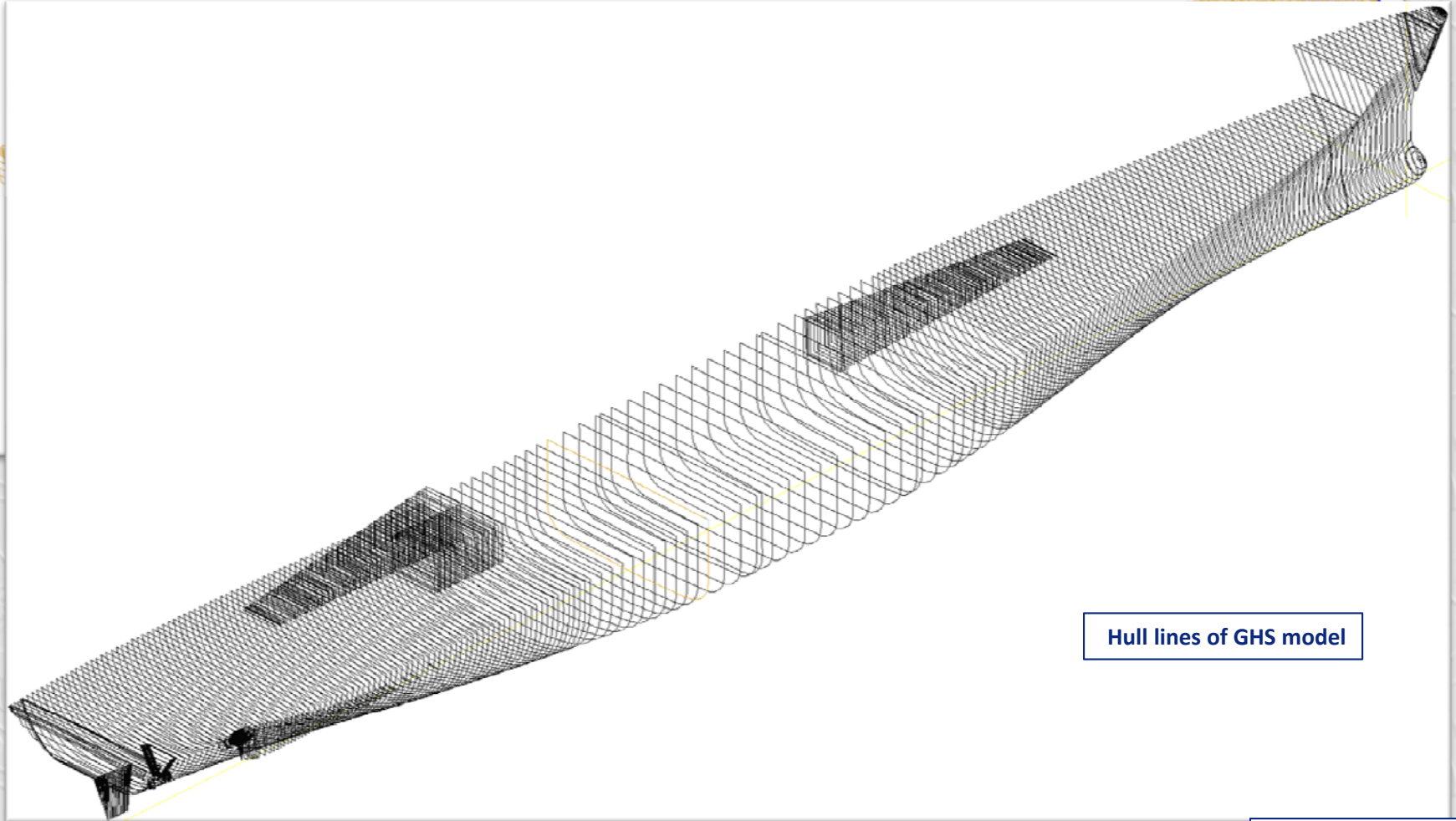


# *Report Outline*

- Introduction
- MSC computer model
- Stability test and uncertainty analysis
- Stability booklet and stability software
- Intact and damage stability
- Hydrostatic sinking analyses
- Ship structures
- Conclusions



# MSC GHS Computer Model



Hull lines of GHS model

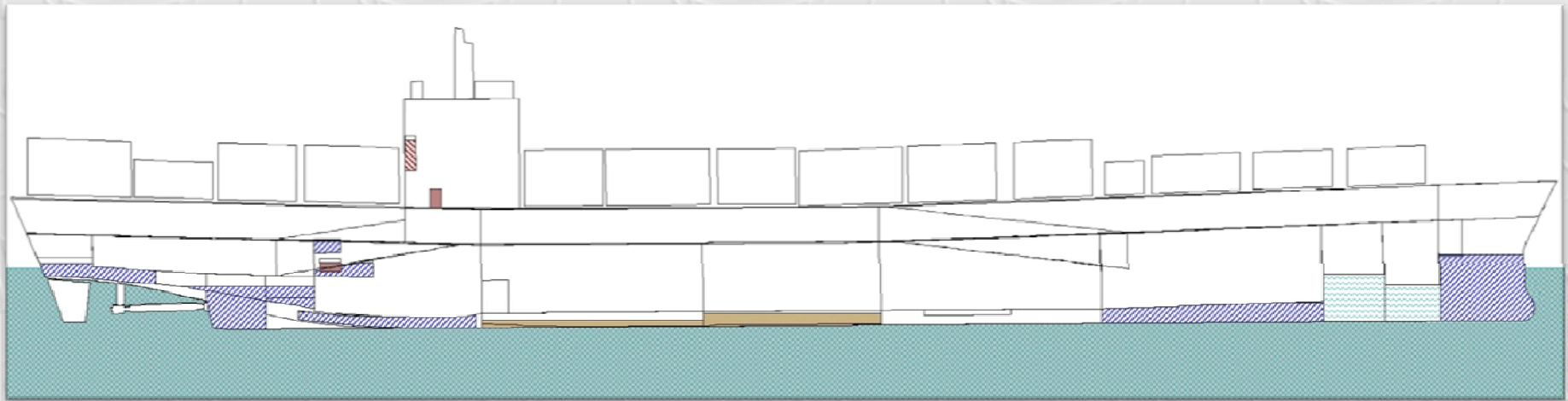
Figures 2-2 to 2-4



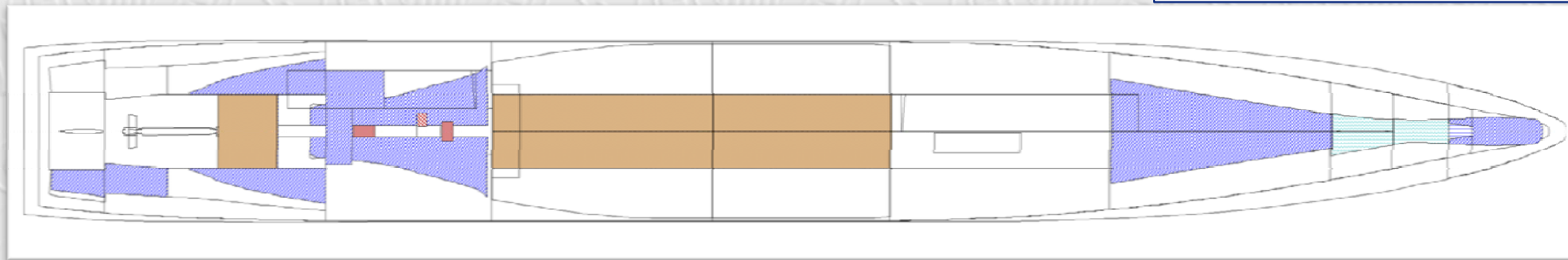


# MSC GHS Computer Model

Profile view – compartments and tanks



Plan view – compartments and tanks







# Stability Test and Uncertainty Analysis

- Stability test

- February 12, 2006 (post-conversion)
- IAW ASTM F1321-92 (2004) guidelines
- Notes
  - Lightship TCG offset in CargoMax
  - Uncertainty in calculated KG and GM values

- Uncertainty analysis

Revised from Preliminary Report

- As-inclined →  $GM = 18.3 \pm 0.2$  ft,  $KG = 26.0 \pm 0.5$  ft
- Lightship →  $KG = 27.8 \pm 0.7$  ft
- Accident voyage →  $KG = 37.3 \pm 0.6$  ft  
 $GM = 4.3 \pm 0.7$  ft

With 95% confidence



# *Stability Booklet and Stability Software*

- Trim & Stability (T&S) Booklet
  - 2007, revised from the 1993 Booklet
    - Modified to account for LO/LO cargo, variable tank data
  - Notes
    - Minimum required GM curves – intact stability criteria only
  
- CargoMax stability and loading software
  - Approved for stability to supplement the T&S Booklet
  - Notes
    - Slack tank requirements in T&S Booklet
    - Approval for loading and ship strength
    - Approval for cargo loading and securing



# *Ship Structures*

- Overall assessment of ship structures
  - Ship structures met regulatory and classification society (ABS) requirements
    - Based on MSC review of documentation available
- CargoMax strength calculations
  - Difference in results vs. MSC analysis
    - Within ABS allowable bending moment
    - Differences in estimated lightship weight distribution
      - Fixed ballast 34% of lightship





# *Intact and Damage Stability*

- Background
  - Righting arms (GZ), righting energy, GM
- Intact stability criteria
  - GM criteria
  - Righting arm (GZ) criteria
- Intact stability assessment of EL FARO
  - GM criteria [applicable]
  - Righting arm (GZ) criteria [if built in 2016]
- Damage stability
  - Damage stability standards
  - Damage stability assessment of EL FARO



# Background: Surface Ship Stability

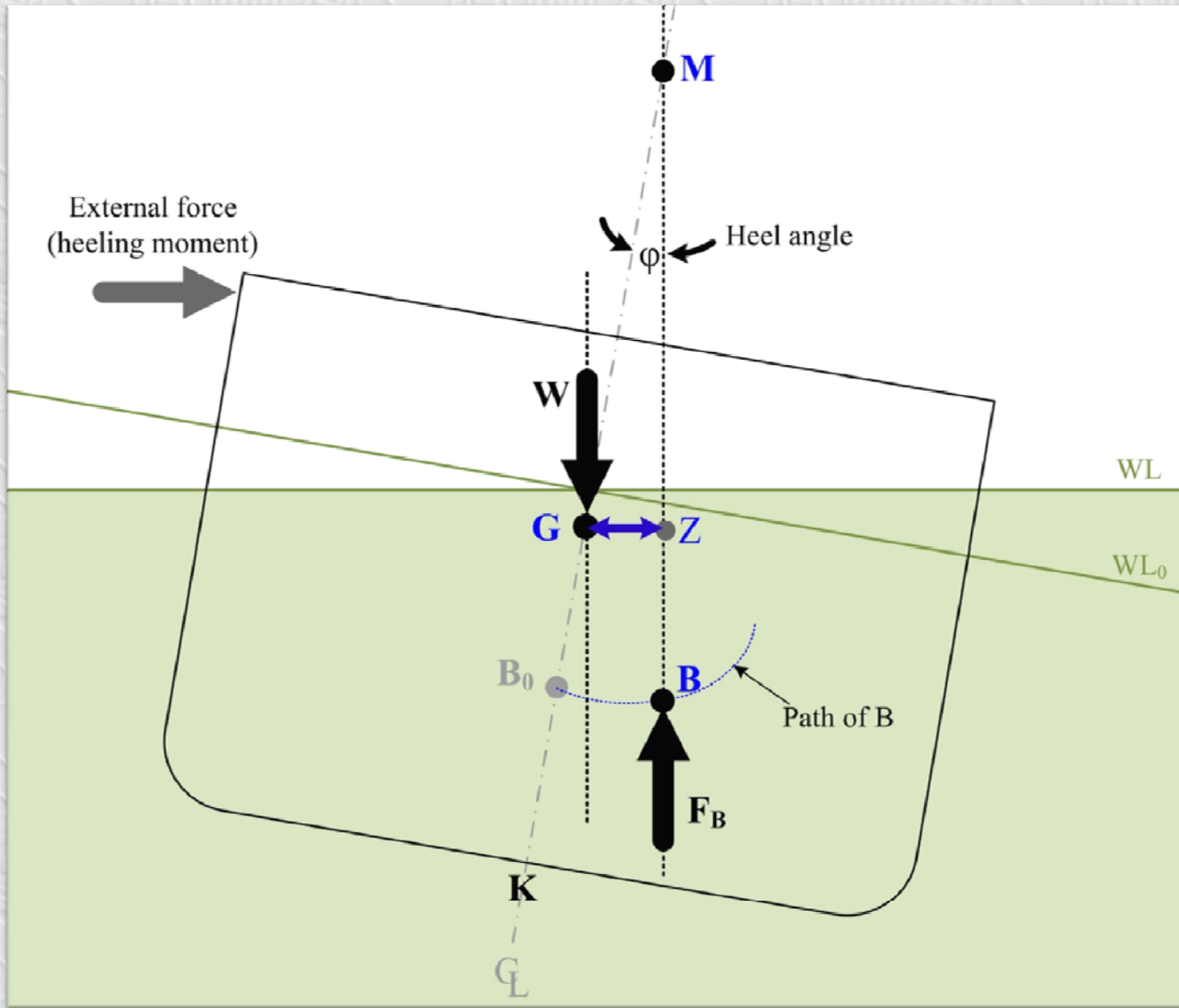
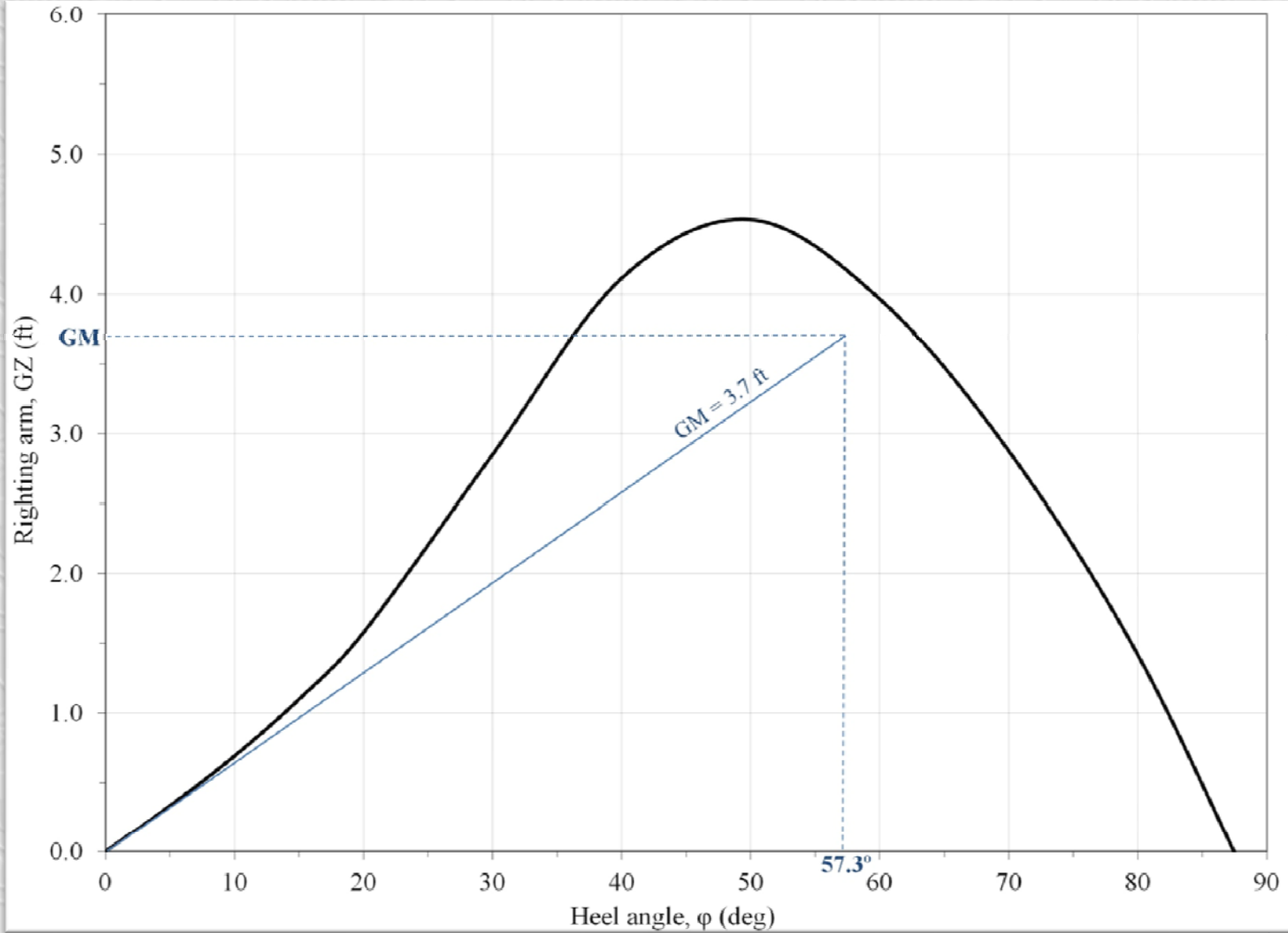


Figure 5-1



# Righting Arm (GZ) Curve and GM







# Righting Arm (GZ) Curves

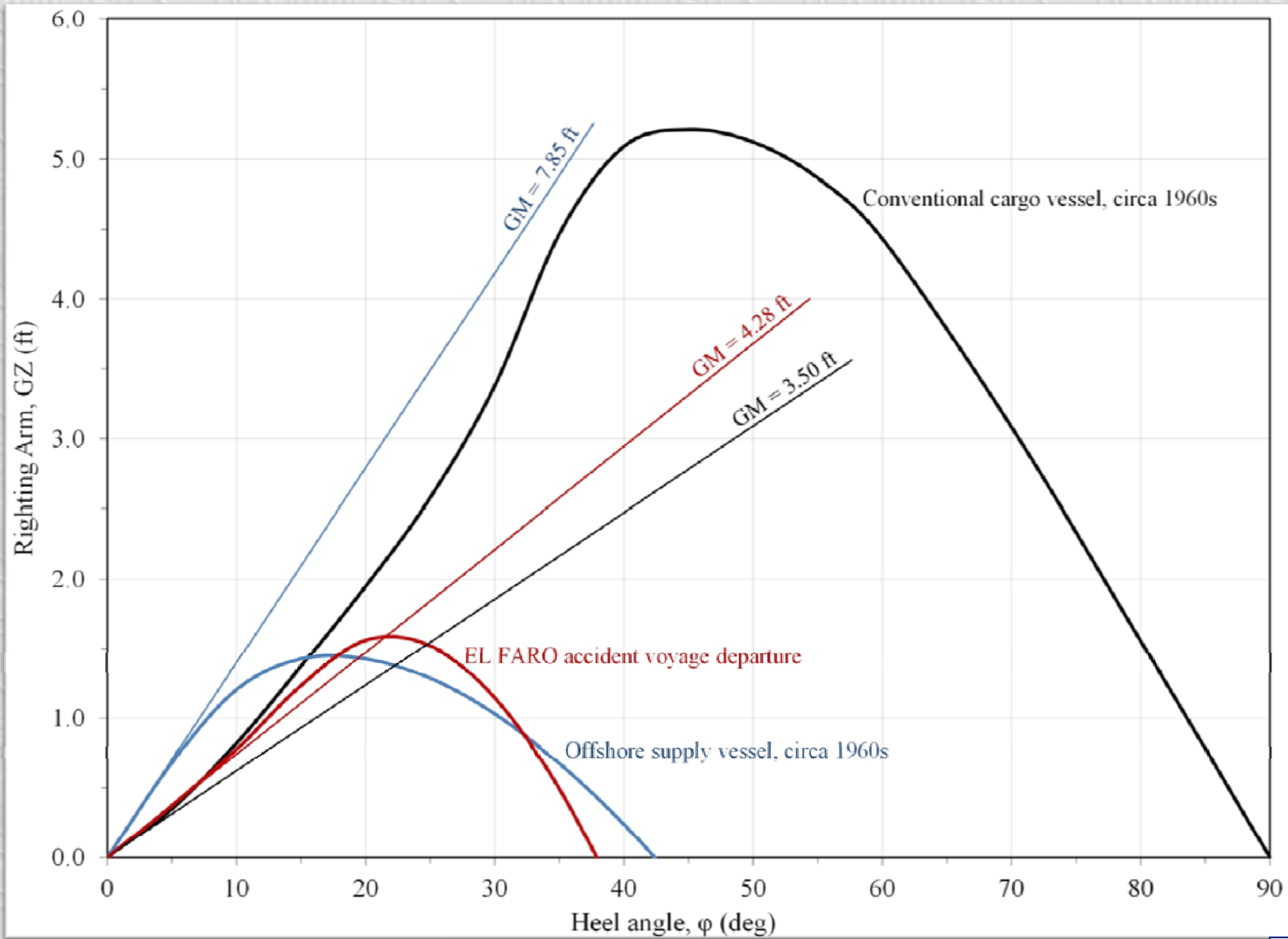
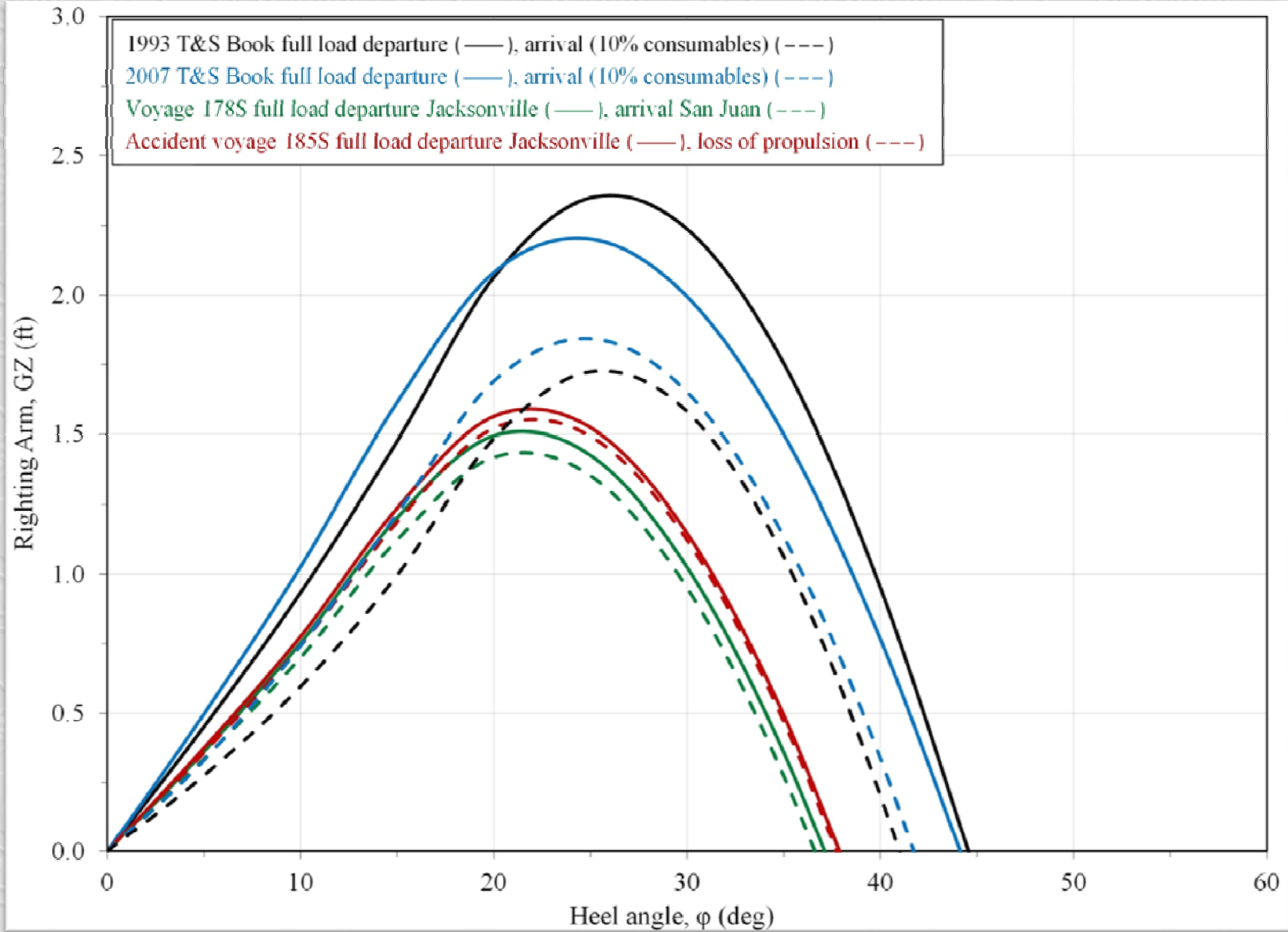


Figure 5-6



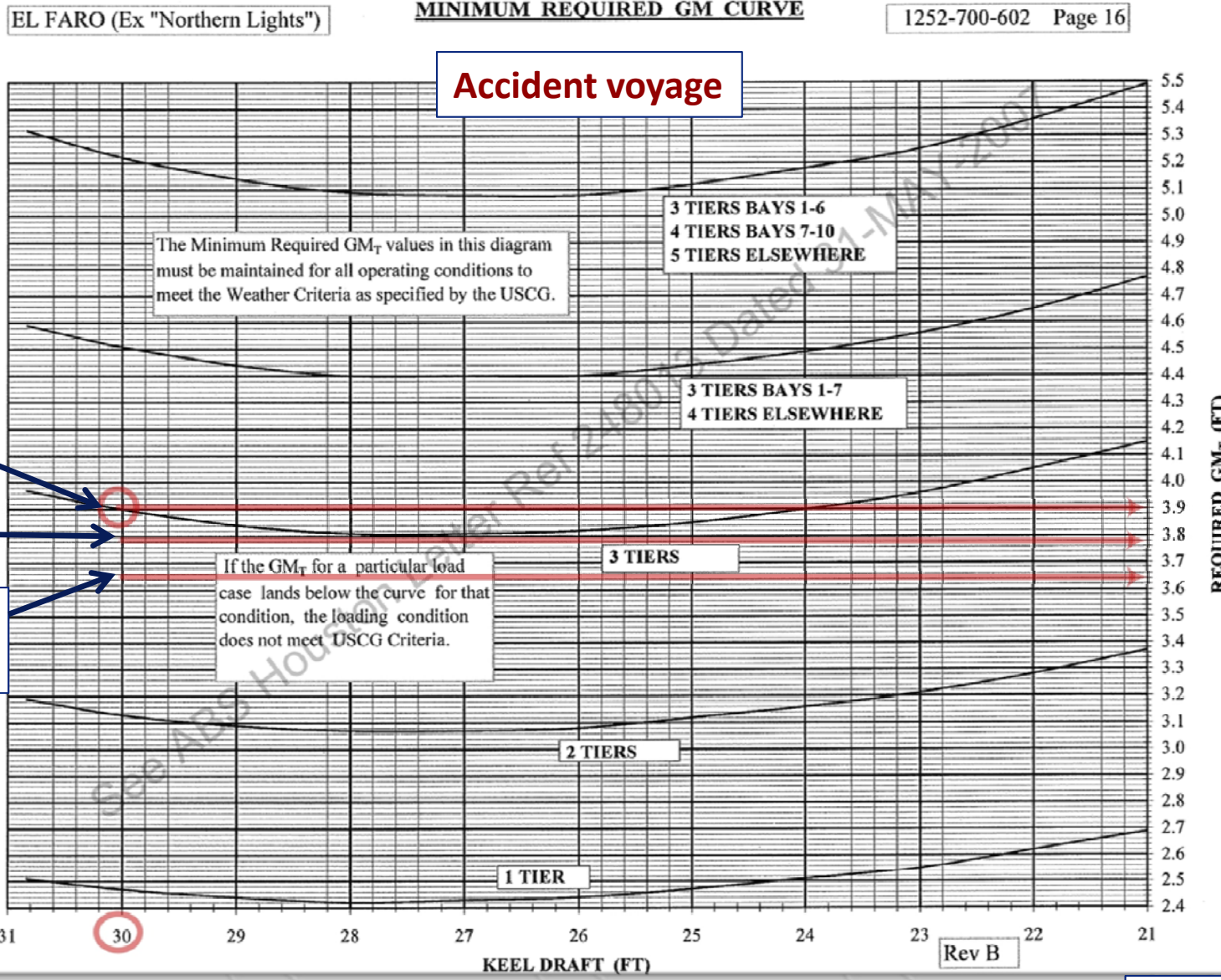
# EL FARO "Benchmark" Loading Conditions





# Intact Stability: GM Criteria

Applicable



T&S Booklet (3 tiers)

MSC GHS calculation

CargoMax "auto windheel" calculation

T&S Booklet

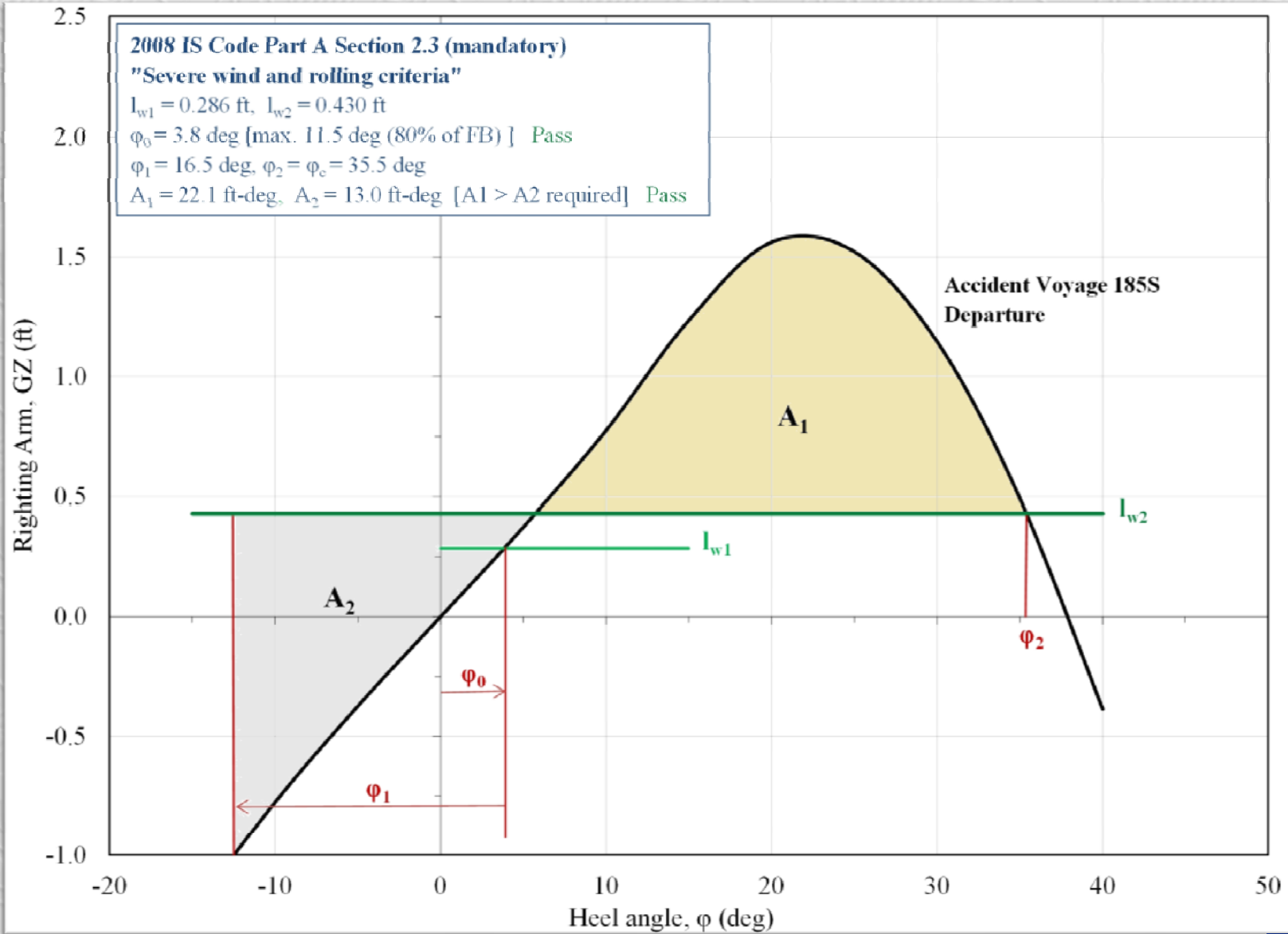
Figure 4-1 (annotated)





# Intact Stability: GZ Criteria

If built in 2016





# Damage Stability

- Damage stability standards
  - SOLAS 1990 (probabilistic)
    - Applicable to EL FARO since 1993 conversion
    - Not completed post-2006 conversion
- MSC analyses
  - SOLAS 1990 [applicable]
  - SOLAS 2009 [if built in 2016\*]
- Results:

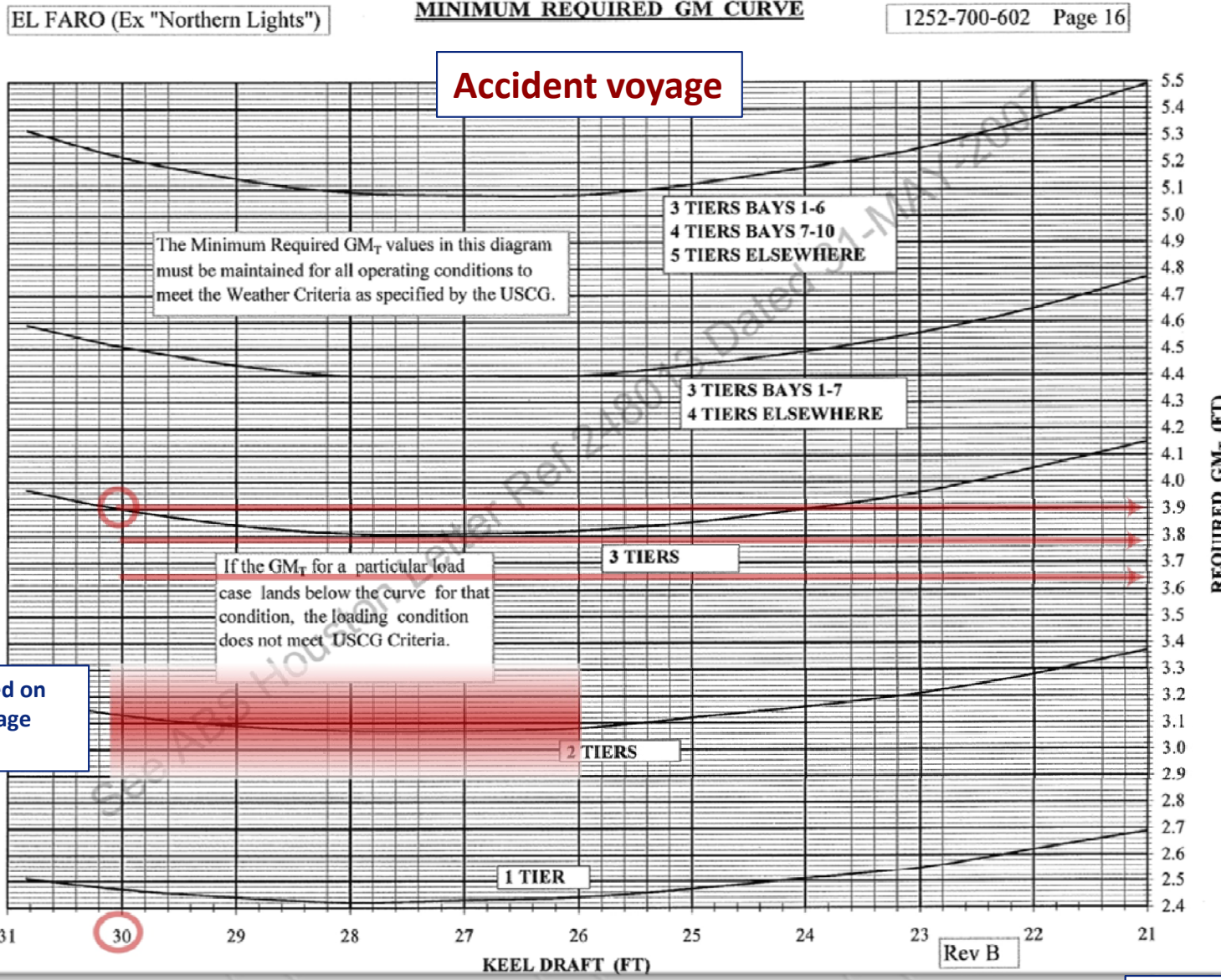
Analysis	SOLAS Standard	GHS Version	Required index (R)	Required GM (feet)
ABS (Gruber, 2016)	1990	8.30	0.600	2.9
MSC	1990	8.50	0.602	3.1
MSC	1990	15.00	0.602	3.3
MSC	2009*	15.00	0.674	5.8

Table 5-3



# Damage Stability

Applicable



Limiting GM based on SOLAS 1990 damage stability analyses

Figure 4-1 (annotated)



# *Hydrostatic Sinking Analyses*

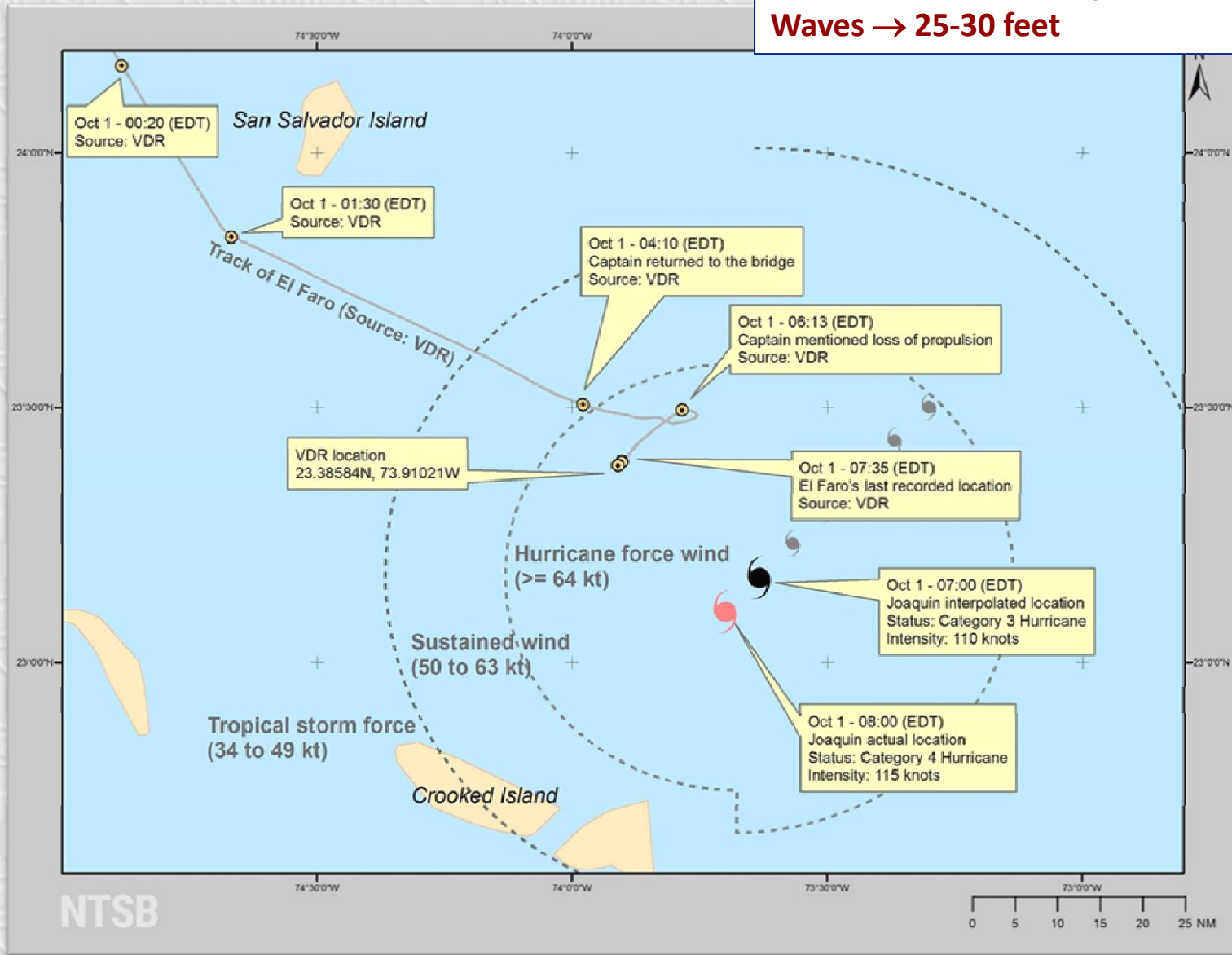
- Environmental conditions
- Potential sources of flooding
- Wind heel effect
- Free surface effect
- Permeability and pocketing effects
- Flooding of Hold 3
- Progressive flooding, downflooding
- Combined effects of wind heel and flooding
- Additional considerations
- Capsizing and sinking





# Environmental Conditions

**Winds → 70-90 knots (sustained)**  
**Waves → 25-30 feet**





## Hold 3 Access Scuttle (Starboard)







# Emergency Fire Pump Piping

Photo of Sister Vessel EL YUNQUE  
(EL FARO similar but not identical)



Figure 6-7



# Cargo Hold Ventilation Openings

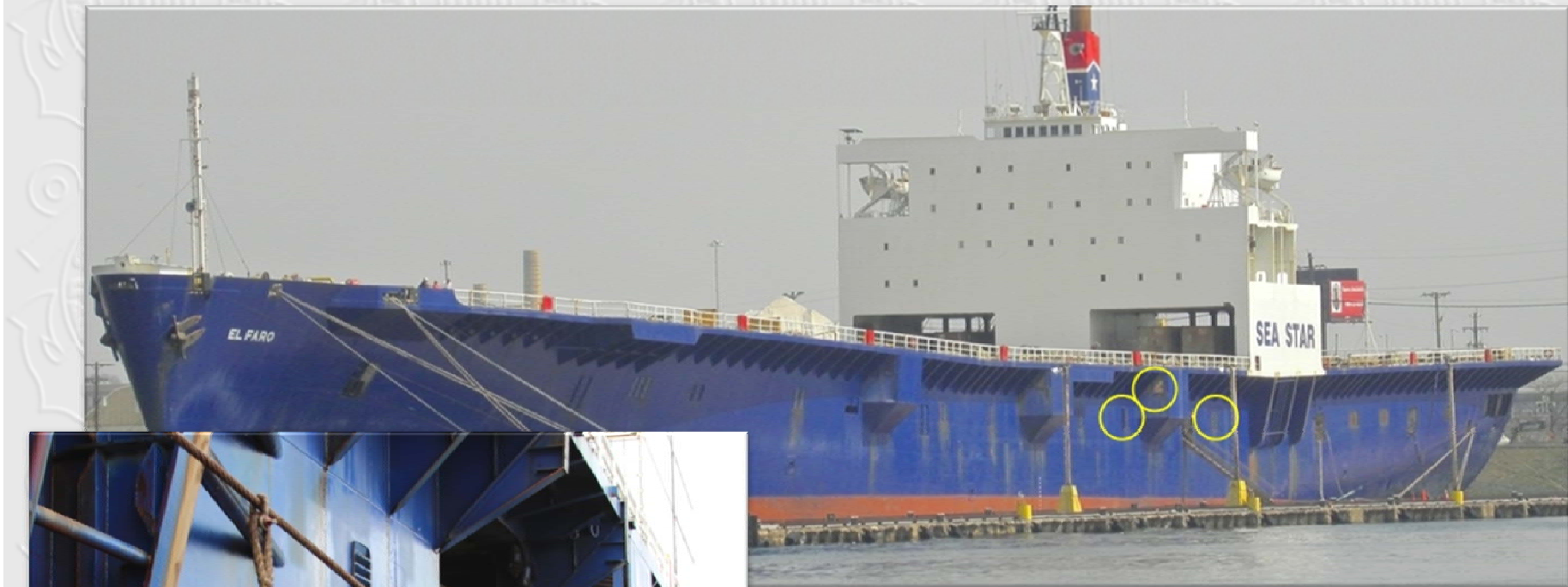


Figure 6-8

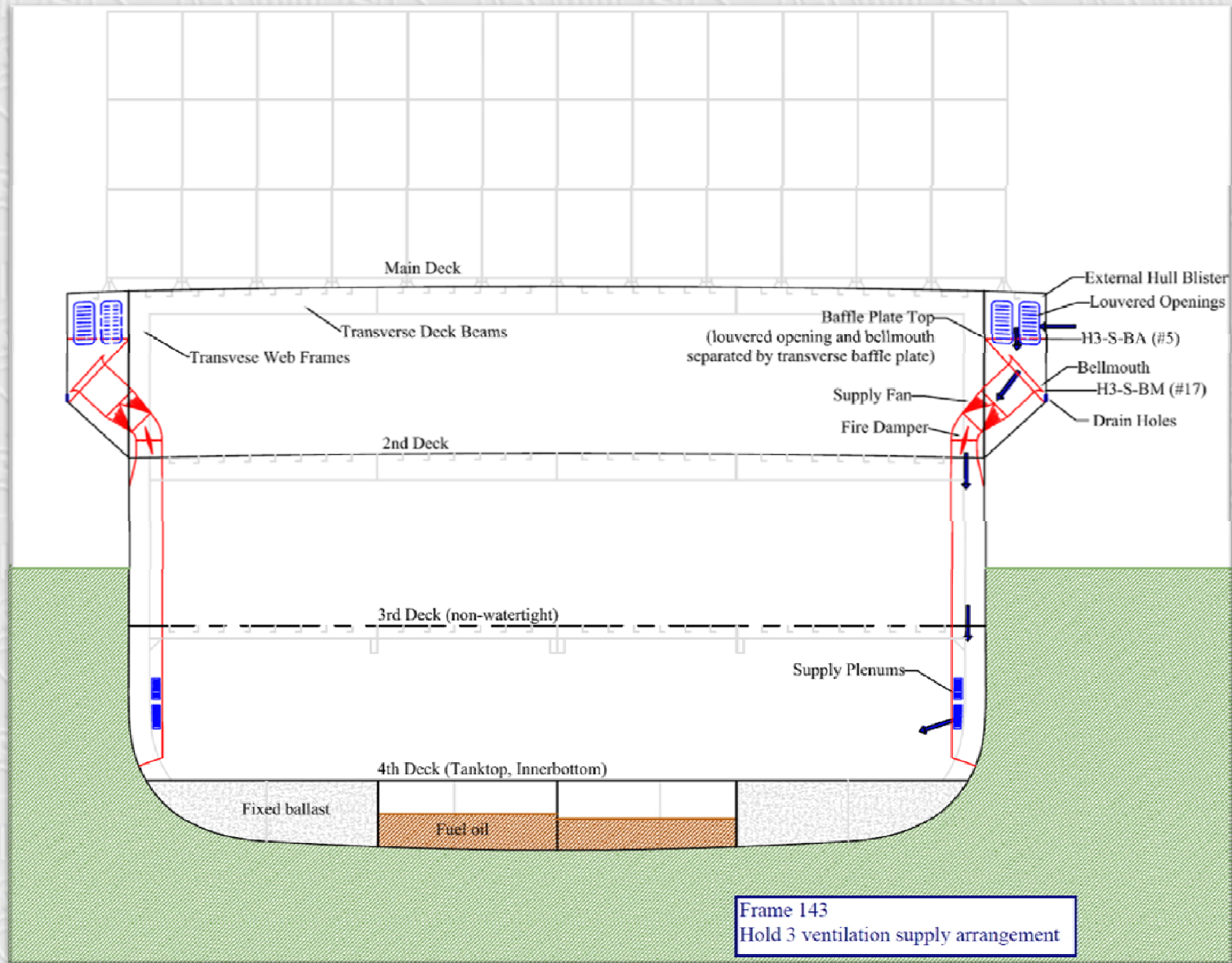


Figure 6-10



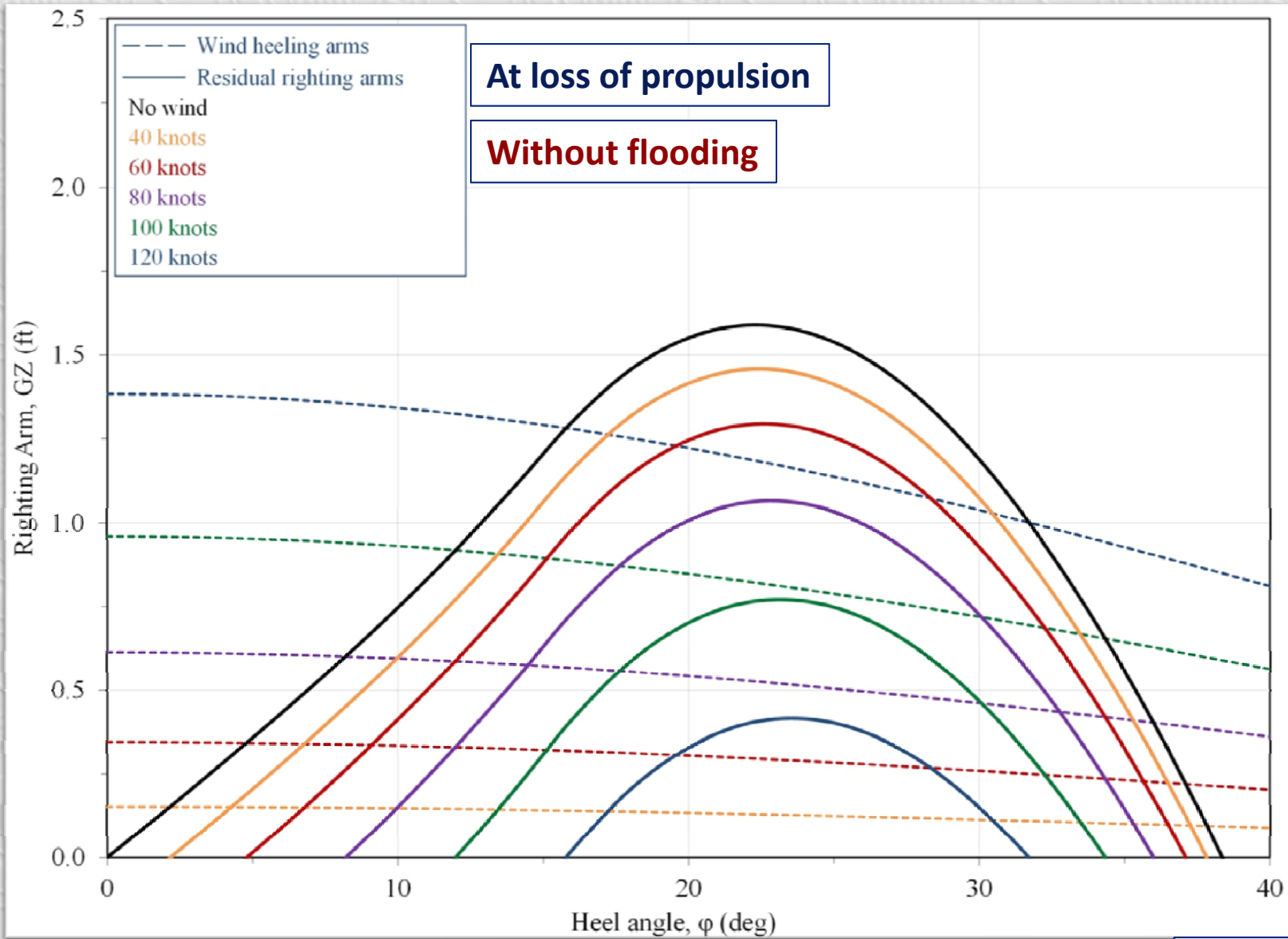


# Cargo Hold Ventilation System





# Wind Heel Effect









# Flooding – Permeability and Pocketing

Frame 143  
Hold 3 ventilation supply  
Hold 3 flooded to 20%  
15 degree heel angle



Cargo lashing tie-downs

Ventilation openings

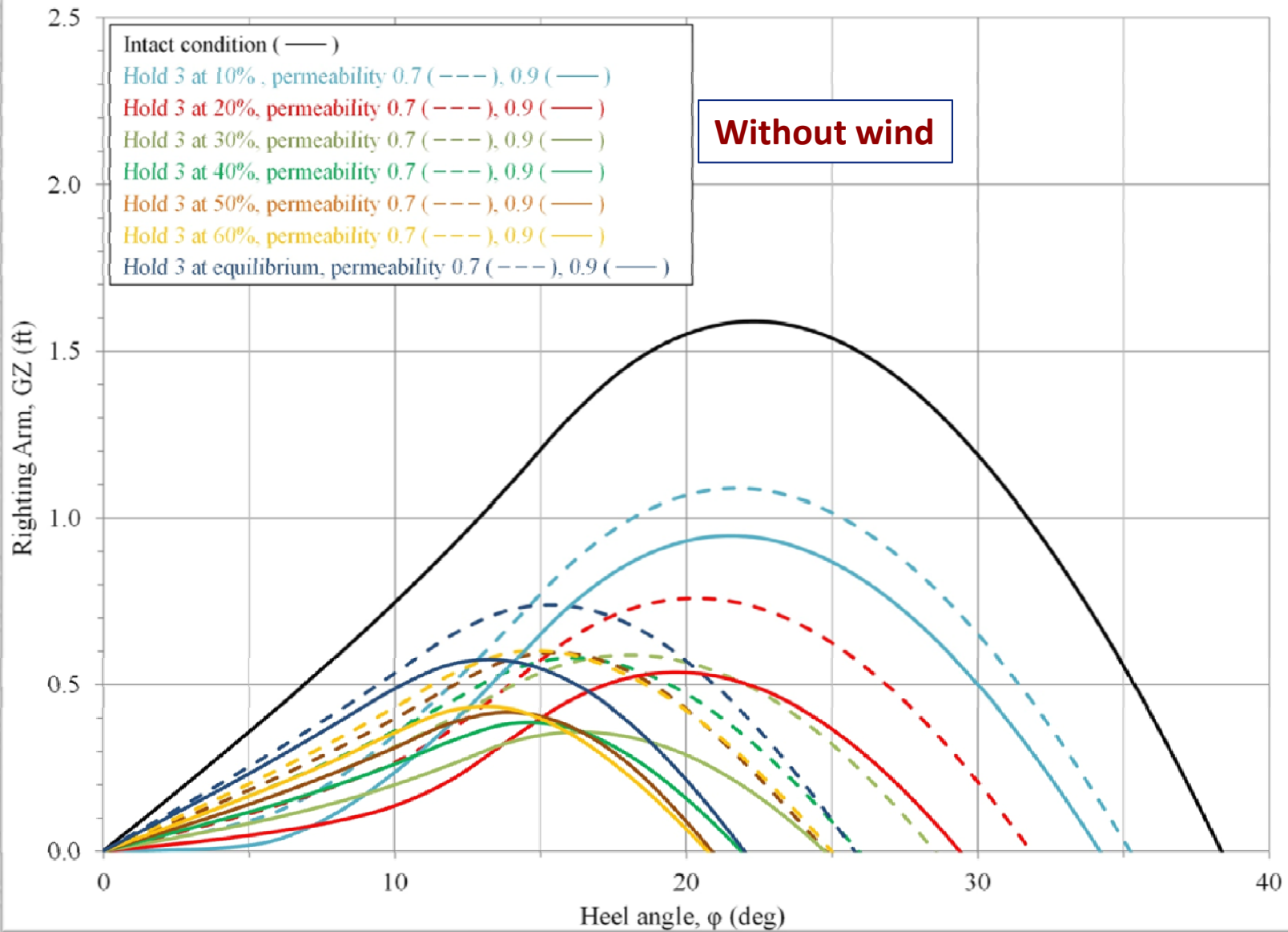
top

7 feet



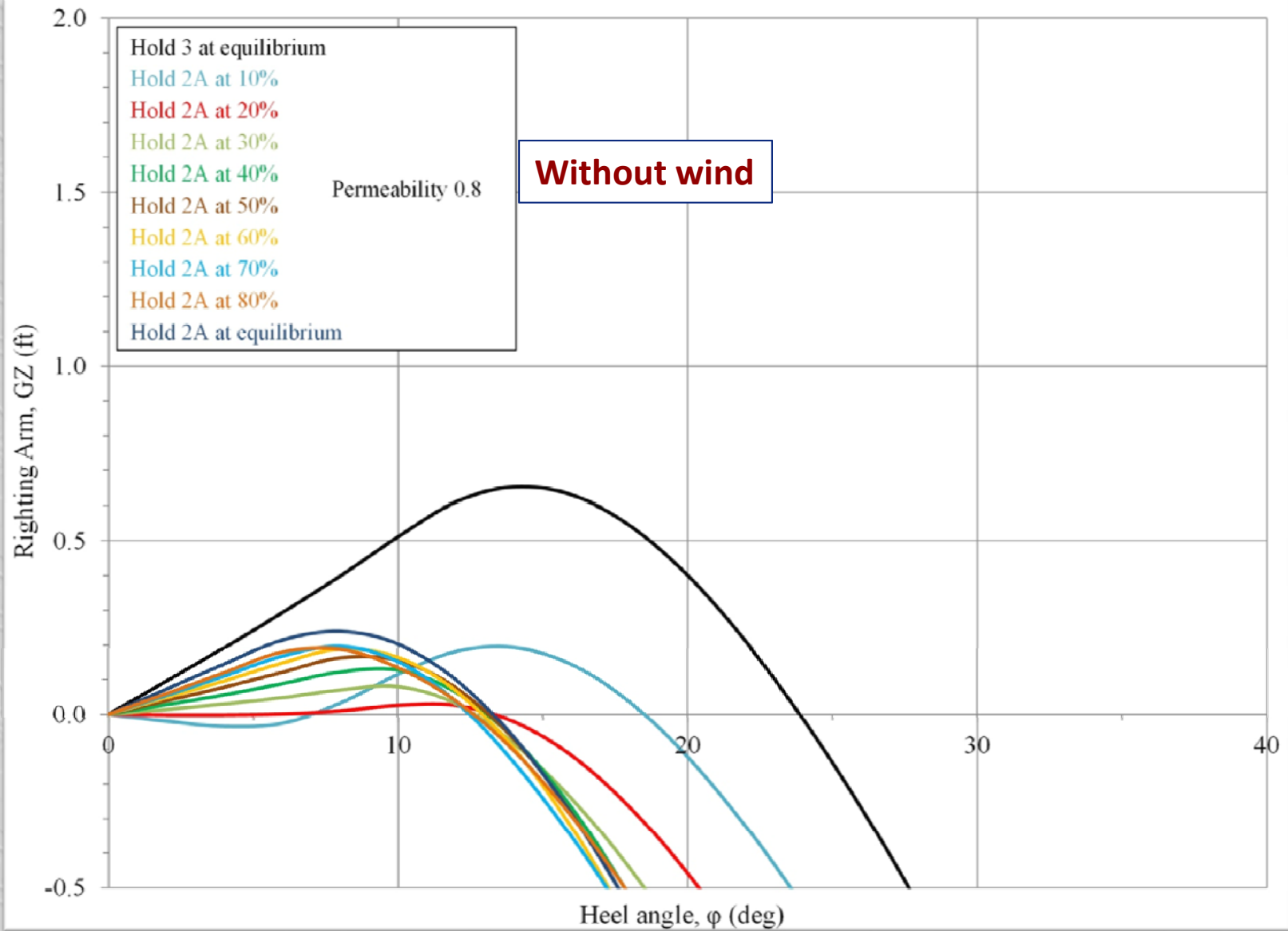


# Flooding of Hold 3



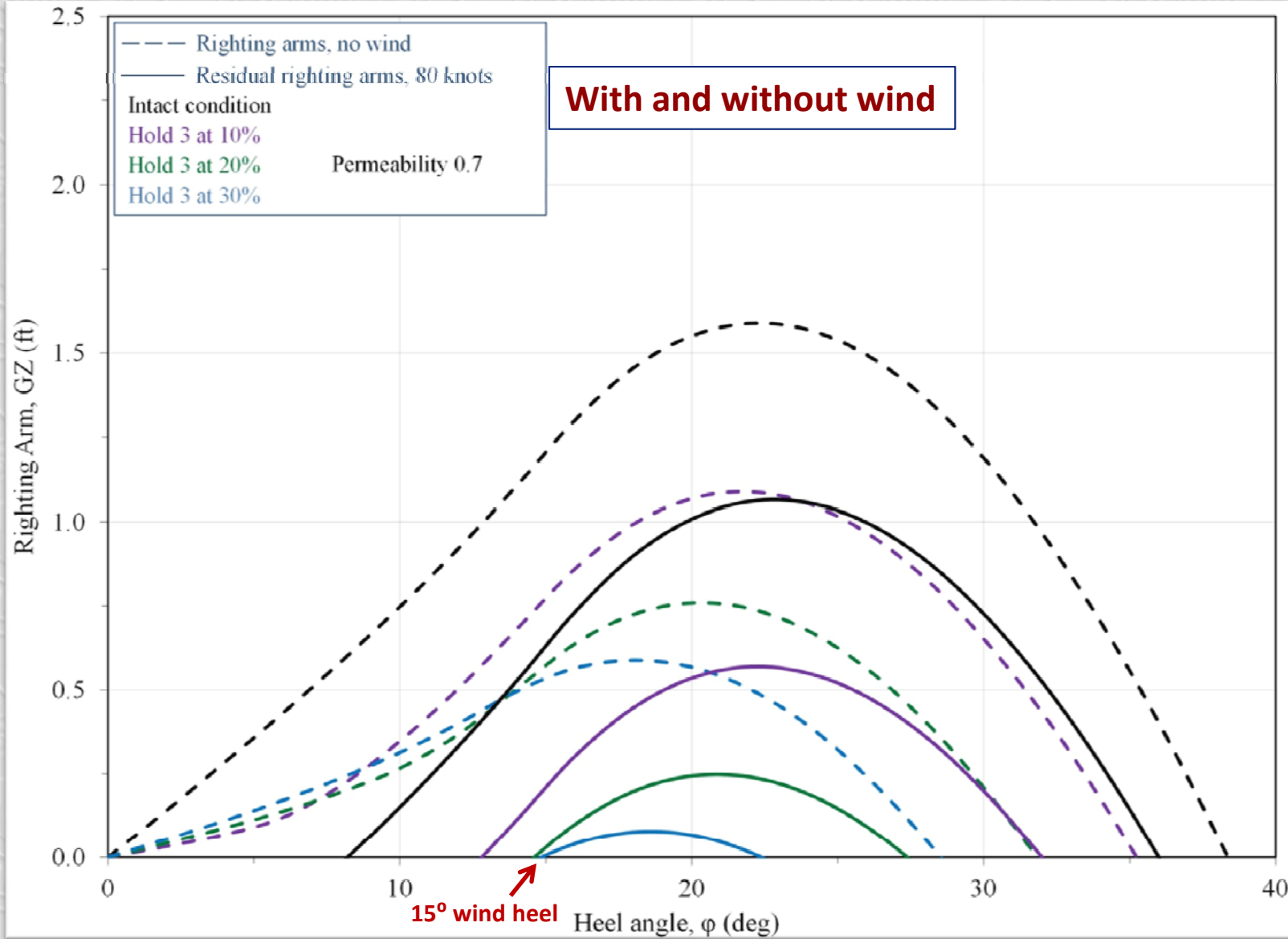


# Progressive Flooding, Downflooding



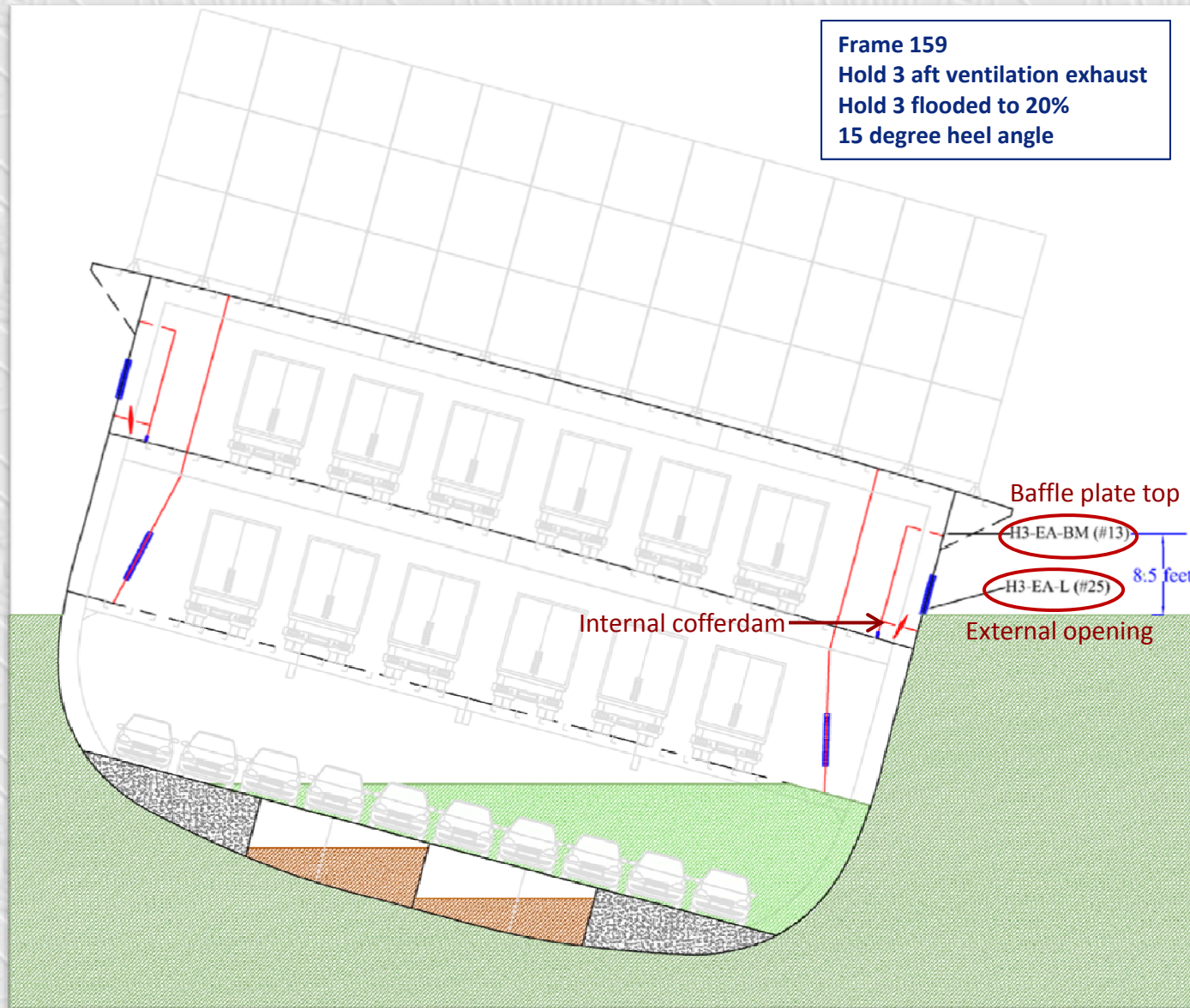


# Combined Wind Heel and Flooding (Hold 3)





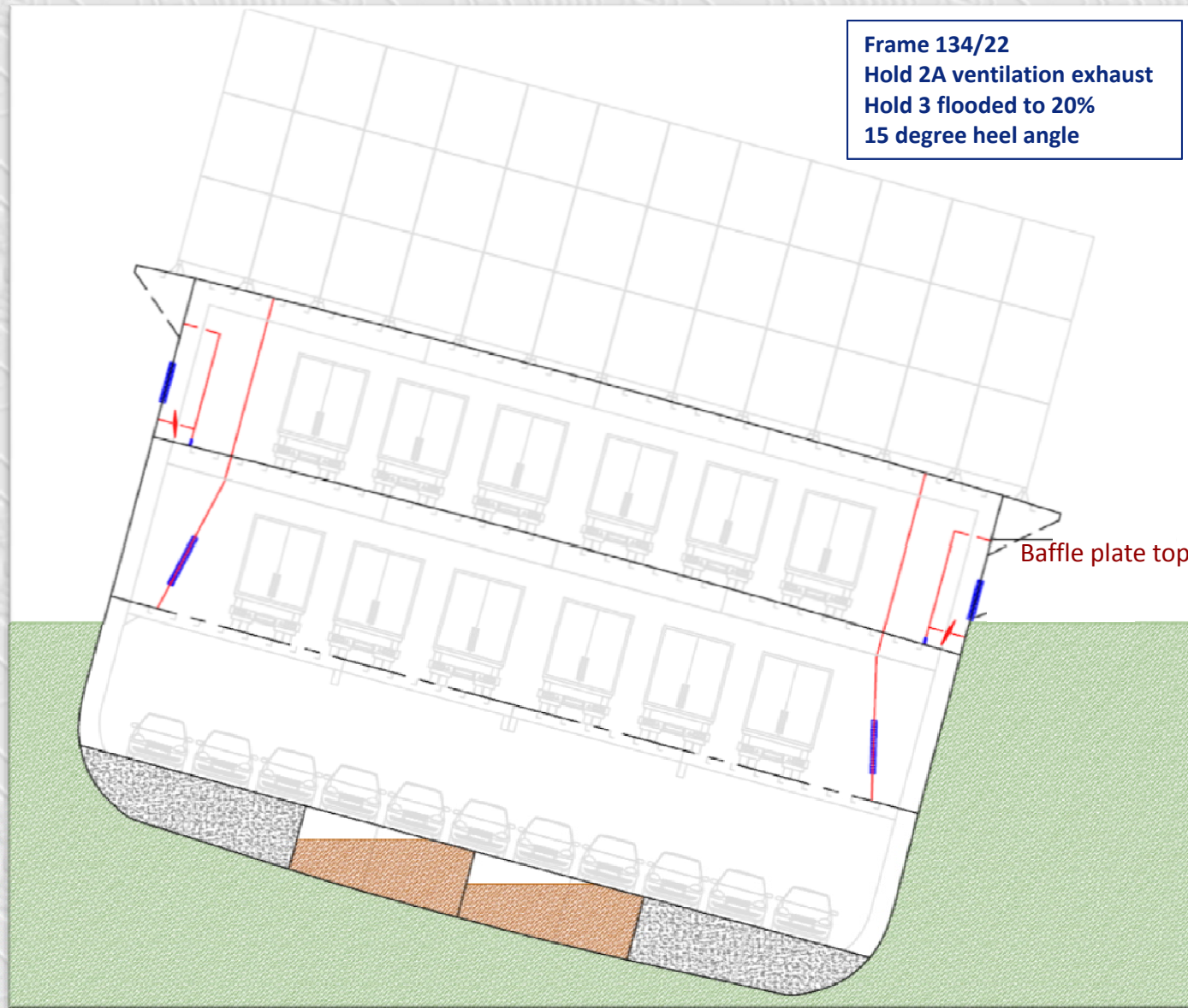
# Combined Wind Heel and Flooding (Hold 3)







# Combined Wind Heel and Flooding





# *Capsizing and Sinking*

- Key considerations
  - Large free surface effect (full-beam cargo holds)
  - Large beam wind heel (70-90 knot winds)
  - Large beam waves (25-30 foot seas)
- Plausible sequence
  - Hold 3 floods, wind heel (→ 15 degrees)
  - Hold 2A floods through vent openings (→ Holds 2, 1)
  - Loss of stability, partial capsize, port main deck awash
  - Loss of containers on deck (arresting full capsize)
  - Continued flooding through port vent openings
  - Vessel sinks
  - Returns ~upright (fixed ballast)



## *Key Conclusions*

- For accident voyage, met applicable intact and damage stability and strength requirements
  - Operated with minimal stability margin, with limited ballast capacity and available freeboard, leaving little flexibility
- Sinking analyses
  - Results highly sensitive to free surface, permeability, pocketing, wind speed effects
  - Ship vulnerable to progressive flooding through cargo hold ventilation openings
  - Unlikely to survive even single-compartment flooding of Hold 3 with combined 70-90 knot winds and 25-30 foot seas
- If built in 2016
  - As operated, would not meet current intact and damage stability standards



# Questions & Answers

